

## Introduction

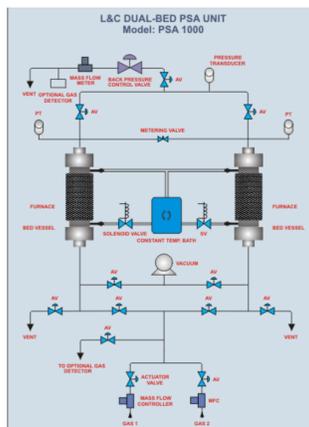
The need to upgrade the quality of CH<sub>4</sub> from diverse sources including coal and biomass gasification, hydraulic fracturing and coal-bed methane has increased in the last 10 years. Among the techniques available for cleaning CH<sub>4</sub>, PSA (Pressure Swing Adsorption) and VSA (Vacuum Swing Adsorption) offer many advantages among them simplicity and economy, especially for remote and small scale operations where other separation techniques are either too costly or impossible to apply.

The gas obtained for the different sources must be upgraded to pipeline quality gas which implies CO<sub>2</sub> and N<sub>2</sub> molar concentrations below 2.5% (1).

Traditionally zeolites and activated carbons had been the adsorbent of choice for CH<sub>4</sub> upgrading but with the discovery of Molecular Gates (2), metal organic frameworks (MOFs) (3,4) and covalent organic frameworks (COFs) (5), the number of possible adsorbents for CH<sub>4</sub> upgrading has substantially increased and with it the need to test these materials under PSA process conditions.

For the purpose of screening adsorbents suitable for CH<sub>4</sub> remediation, a fully automated dual bed PSA/VSA was designed and constructed that allows for small adsorbent beds and flexibility of experimental parameters of flow, pressure, temperature and cycle times. The system's performance will be demonstrated by the separation of N<sub>2</sub> and CO<sub>2</sub> from a CH<sub>4</sub> stream using a commercial 13-X zeolite adsorbent. The effects of pressure, temperature, cycle time, purge and vacuum on the separation efficiency will be also presented.

## Experimental: Instrument and Adsorbent Media



The PSA/VSA system used in the breakthrough and cycling experiments was a dual-bed system (Model PSA-1000 from L & C Science, Hialeah, FL, USA). A description of the system is given in Figure 1.

The adsorbent used was a 13-X zeolite material from Sigma-Aldrich Chemicals. The zeolite particles were spherically shaped with diameters ranging from 1.4 to 2 mm (Tyler MESH sizes 8 to 12). The isotherms for this material with N<sub>2</sub>, CH<sub>4</sub> and CO<sub>2</sub> at 298 and 308 K and pressures up to 1300 kPa are shown in Figure 2.

Figure 1. Schematic of the PSA System

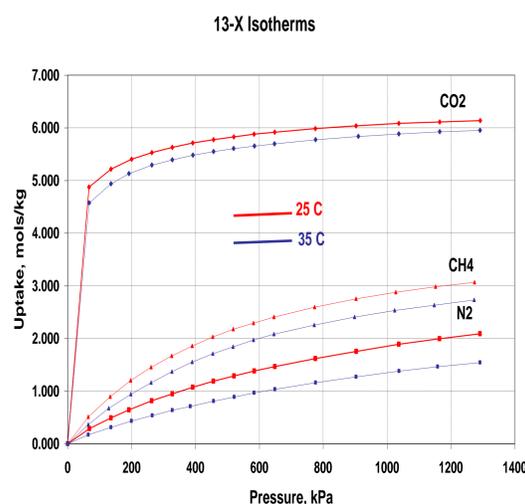


Figure 2. CH<sub>4</sub>, CO<sub>2</sub> and N<sub>2</sub> Isotherms for 13-X

The characteristics of the two adsorption beds are given in Table 1.

Bed Diameter, m	0.0211
Bed Active Length, m	0.718
Bed Density, kg/m <sup>3</sup>	676
Adsorbent Volume, m <sup>3</sup>	2.5x10 <sup>-4</sup>

Table 1. Adsorption Bed Properties

## PSA Runs

The gas composition selected, 60% CH<sub>4</sub>, 20% CO<sub>2</sub> and 20% N<sub>2</sub>, was the same used by Cavenati *et al* (1) in their PSA/VSA work. Six different runs were carried out with the same total flow rates for the feed (2SLM), adsorption pressure (500 kPa), purge (0.1 SLM) but different cycle times, blow down sequence and two different temperatures: 298 K and 318 K. In one series of experiments the system was blow down to a pressure of 20 kPa right after the adsorption or feed step and in the other series the two beds were pressure equalized before one was blow down and the other pressurized. A representation of the two cycle configurations is given in Figure 3.

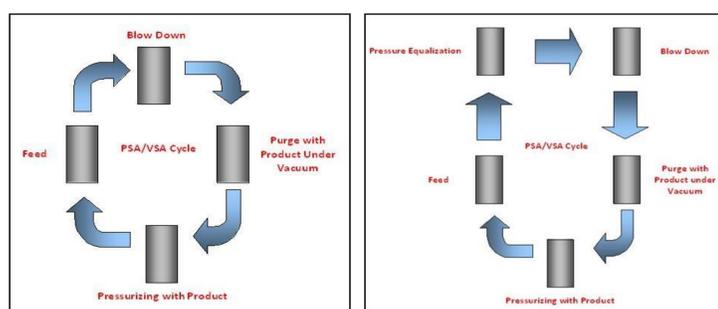


Figure 3. PSA Cycle

## Results

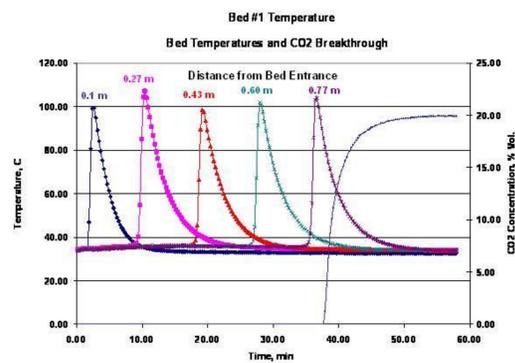


Figure 4. Breakthrough Curve for CO<sub>2</sub> and Bed Temperatures

The first experiment was to determine the breakthrough for CO<sub>2</sub> at 5 bars, 298 K and a concentration of 20% and 80% CH<sub>4</sub>. The total flow rate of the gas was 2 SLM. In Figure 3 the breakthrough experiment is shown (for CO<sub>2</sub> only) together with the temperature rise in the zeolite bed.

In Figure 5 and 6 bed pressures and bed temperatures are shown for run 4 (The different runs are listed in Table 2).

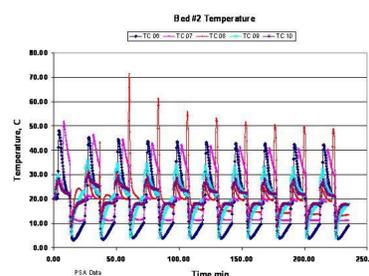


Figure 5. Temperature profile in Bed #2 for Run #4

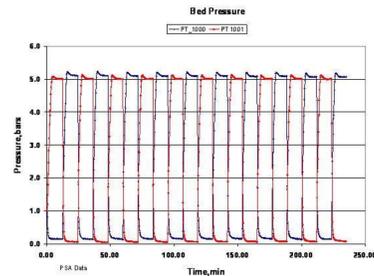


Figure 6. Pressure During Cycling for Run #4

Run	Pressurization, s	Feed, s	Purge, s	Product, CO <sub>2</sub> , %	CH <sub>4</sub> Recovery, %	T, K
1	195	195	250	0.0	63.5	298
2	180	600	550	0.0	82.0	298
3	75*	300	250	0.1	82.9	298
4	75*	600	550	0.1	95.6	298
5	60*	300	250	0.2	88.2	318
6	60*	600	550	0.5	97.8	318

\*Runs with Pressure Equalization Prior to Blow Down

Table 2. Results of the PSA runs with zeolite 13-X at 500kPa and 2 SLM flow

## Conclusions

From Table 2 one can conclude the following regarding the PSA process:

1. Increasing the feed time improves the bed utilization and CH<sub>4</sub> recovery without impacting on the CO<sub>2</sub> concentration in the product.
2. By pressure equalization prior to blow down and purge one can substantially increase the CH<sub>4</sub> recovery without impacting on the CO<sub>2</sub> concentration.
3. The best results in terms of CH<sub>4</sub> recovery are obtained with longer feed times and pressure equalization.
4. Although the CO<sub>2</sub> concentration in the product is very low, still the overall purity of the process gas is not much higher than 80% in all these runs because of the fast breakthrough of N<sub>2</sub>.
5. The lab-sized PSA system it is very well suited for the purpose of screening materials for CH<sub>4</sub> upgrading and for optimization of the PSA/VSA process.

## References

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